Modeling the mechanics of HMX detonation using a Taylor–Galerkin scheme

Adam V. Duran, Veera Sundararaghavan *
Department of Aerospace Engineering, University of Michigan, Ann Arbor, MI 48109, USA

**Highlights**

- An integrated algorithm for cyclotetramethylene tetranitramine (HMX) particle detonation that incorporates equations of state, Arrhenius kinetics, and mixing rules.
- A stabilized Taylor–Galerkin finite element simulation algorithm with pressure and temperature equilibriums enforced across phases.
- The scheme captures the distinct features of detonation waves: rarefaction wave, contact discontinuity, shock wave, and the von Neumann spike.
- Computed detonation velocity compares well with experiments reported in literature.

**Abstract**

Design of energetic materials is an exciting area in mechanics and materials science. Energetic composite materials are used as propellants, explosives, and fuel cell components. Energy release in these materials is accompanied by extreme events: shock waves travel at typical speeds of several thousand meters per second and the peak pressures can reach hundreds of gigapascals. In this paper, we develop a reactive dynamics code for modeling detonation wave features in one such material. The key contribution in this paper is an integrated algorithm to incorporate equations of state, Arrhenius kinetics, and mixing rules for particle detonation in a Taylor–Galerkin finite element simulation. We show that the scheme captures the distinct features of detonation waves, and the detonation velocity compares well with experiments reported in literature.

© 2016 The Authors. Published by Elsevier Ltd on behalf of The Chinese Society of Theoretical and Applied Mechanics. This is an open access article under the CC BY-NC-ND license (http://creativecommons.org/licenses/by-nc-nd/4.0/).

Energetic composite materials are used as propellants, explosives, and fuel cell components. During the detonation of these materials a shock wave is sustained by the rapid chemical energy heat release involving tightly coupled nonlinear interactions between chemistry and mechanics. These waves have extreme features which laboratory experiments are seldom equipped to handle; they travel at typical speeds of several thousand meters per second and the peak pressures can reach about 100 GPa [1]. Currently, there is significant interest in engineering the microstructures of these energetic composites for targeted shock sensitivity and energy output. Literature in this area indicate the importance of composite features, for example, smaller energetic particles have lesser run time to detonation [2] and the time to detonation increases with the strength and content of the matrix (binder) material [3]. The first step in understanding these effects is the development of a reliable computational model of the energetic particle, typically the energetic crystal cyclotetramethylene tetranitramine (HMX), in these composites.

Modeling reactive burn of extreme detonation events is a significant challenge. The model is highly dependent on experimental data for each explosive composition. Unreacted material is converted to detonation products by a finite reaction rate where intermediate reactive species only exist for a few nanoseconds and are extremely difficult to measure experimentally. Reactive burn models are typically pressure (e.g. Ref. [4]) or temperature dependent (e.g. Arrhenius model). Arrhenius reaction kinetics are often approximated in a single step [5] and are tuned to experiments and chemical data such as heats of formation [6–8]. Equations of state are defined for each of the reaction states and mixing rules are needed for partially reacted states. Typically for the pressure dependent models, pressure equilibrium is assumed [9] or an analytic mixture is used [10] for partially burned mixture of reactants and products. For temperature based Arrhenius models, it is assumed that the unreacted explosive and reac-
tion products are in both temperature and pressure equilibrium. Although timescales of interest suggest that pressure equilibrium is reached long before temperature equilibrium, both temperature and pressure equilibrium is used in this work. This assumption is widely used \cite{5,11} and will affect partially reacted pressures and temperatures.

Shock strength of HMX is typically an order of magnitude higher than its yield strength. The material response of HMX for the unreacted explosive and the explosive products. These equations are written as a function of specific volume $v$ and energy $e$. They are related to the state variables as follows:

$$v = 1/\rho, \quad e = E - (1/2)(u^2 + v^2).$$

The pressure and temperature for a solid unreacted material are given by a linear Mie–Grüneisen EOS and those for the gaseous reaction products are in temperature and pressure equilibrium; i.e., $T = T_e(v_e, e_e)$ and $p = p_e(v_e, e_e) = p_e(v_e, e_e)$. Equilibrium is enforced by iterating on $v_e$ and $e_e$. The following system can be solved using a Newton–Raphson method.

$$\begin{align*}
p_e - p_s & = \left[ \frac{\partial p_e}{\partial v_s} \frac{\partial p_e}{\partial v_e} \frac{\partial p_e}{\partial e_s} \frac{\partial p_e}{\partial e_e} \right] \delta v_e. \end{align*}$$

To relate the unreacted solid and reaction products, a mixture rule is used, $\nu = (1 - \lambda)v_s + \lambda v_e$ and $e = (1 - \lambda)e_s + \lambda e_e$. Here, $\lambda$ is the burn fraction; the mass fraction of detonation products in the mixture. For the one-step reaction in this work, $\lambda = N_B$. Now, the system of equations is closed and both EOS can be expressed in terms of the solid specific volume and internal energy. Convergence is achieved when $\Delta p < 10^{-4}$ Mbar (1 bar = 10^5 Pa) and $\Delta T < 10^{-4}$ K as discussed in Ref. \cite{11}.

The 2D reactive Euler equations given by Eq. (1) are solved using a one-step DG scheme. This widely used time-stepping algorithm is second-order accurate, explicit and analogous to the Lax–Wendroff method \cite{20}. Taking a Taylor series expansion of $U$ from Eq. (2) in time,

$$U^{n+1} = U^n + \Delta t U^n + \frac{1}{2} \Delta t^2 U^n + \Theta(\Delta t^3),$$

where $\Delta t$ is the time step, superscripts $n + 1$ denotes the current time and $n$ denotes the previous time. The second term of the right hand side of Eq. (5) is found from rearranging Eq. (1) and the third term is found by differentiating Eq. (1) with respect to time. Now Eq. (5) is written as

$$U^{n+1} = U^n + \Delta t (S - (F_1)_{x} - (F_2)_{y}) + \frac{1}{2} \Delta t^2 [S_{x} - (A_1 S - A_1^2 U_s - A_1 A_2 U_y)_{x}] + \frac{1}{2} \Delta t^2 [S_{y} - (A_2 S - A_1 A_2 U_s - A_2^2 U_s)_{y}] +$$

At each time step, the equations of state and the mixing rule is used to compute $A_i$ and the source terms. The field variables are solved.
using the weak form given as follows:

\[
\int \int W \frac{U_{n+1} - U_n}{\Delta t} \, dA = \int \int W S^n \, dA + \int \int (W_x F_1 + W_y F_2)^n \, dA + \frac{1}{2} \Delta t \int \int W S^n c_x^n \, dA + \frac{1}{2} \Delta t \int \int W (A_1 X - A_1^2 U_1 - A_1 A_2 U_2)^n \, dA + \frac{1}{2} \Delta t \int \int W (A_2 S - A_2 A_1 U_1 - A_2^2 U_2)^n \, dA - \int \left[ W (F_1^n + \frac{1}{2} \Delta t F_1^n) \right]_{y_i}^{y_f} \, dy - \int \left[ W (F_2^n + \frac{1}{2} \Delta t F_2^n) \right]_{x_i}^{x_f} \, dx.
\]

(7)

To ensure stability in regions of compression where \(\partial u/\partial x < 0\) and \(\partial v/\partial y < 0\), flux is computed based on a group representation. After Galerkin spatial discretization the algebraic equation \(M(U^{n+1} - U^n) = B^n\) is obtained and solved for \(U^{n+1}\). A lumping scheme is then used for the purpose of adding numerical dissipation and to give non-oscillatory solutions in the presence of steep solution gradients \([26]\). Here, the consistent mass matrix \(M\) is replaced by the diagonal matrix \(\hat{M}\), obtained by row sum. The mass lumping reduces the second order TG scheme to a first order scheme. Addition of a small first order solution adds an artificial numerical dissipation to the system. The smoothed solution is obtained by adding a small dissipation through parameter \(d\), where \(0 \leq d \leq 1\); for maximum dissipation \(d = 1\). The smoothed solution is obtained as

\[
\hat{M}^i (U^{\text{smooth}} - U^n) = (M - \hat{M}^i) U^{n+1},
\]

(8)

where \(d\) is locally constructed by considering pressure gradients as expressed in the equations below. Here, nodes “i” are connected to nodes “j” where \(p_{ij}\) denotes local pressure and \(x_{ij}\) denotes local position.

\[
d_i = \left| \frac{p_j - 2p_i + p_{i-}}{p_j + 2p_i - p_{i-}} \right|, \quad d_j = \left| \frac{p_{i+} - 2p_i + p_{i-}}{p_{i+} + 2p_i - p_{i-}} \right|,
\]

(9)

where

\[
p_{i-} = p_i - 2(x_i - x_j) \cdot [\nabla p]_i,
\]

\[
p_{i+} = p_i - 2(x_i - x_j) \cdot [\nabla p]_i.
\]

(10)

Then, the artificial viscosity coefficient for segment i-j is determined by the following equation, where \(\chi\) is a free parameter discussed in the following section.

\[
d_{ij} = \min \{ \chi \max (d_i, d_j), 1 \}.
\]

(11)

3. Verification using SOD shock benchmark problem

To test the stability and accuracy of the scheme described above, the classical fluid dynamics shock tube problem is solved \([27]\). The test consists of two fluids at differing pressures separated by a membrane. Once the membrane is removed, a rarefaction wave contact discontinuity and shock wave is formed. The solution for an ideal gas is obtained analytically using Riemann invariants and is compared with numerical results in Fig. 1. The numerical results in Fig. 1 show good agreement with the exact solution and the distinct characteristic signatures of the test are captured. Next, the effects of the free parameter \(\chi\) on the numerical solution are studied. Figure 2 shows the average error per node as a function of the parameter \(\chi\) for two different time steps. In general, error increases with increasing the parameter \(\chi\) and decreasing the time step increases the average error per node. The optimal parameter for both time steps is \(\chi = 0.1\), the value used in Fig. 1 and in subsequent sections.

4. Reactive HMX models in 1D and 2D

Next, shock loading a single HMX sample is studied. Numerical results are obtained with linear elements for a 1 cm domain with \(\Delta x = 0.01\) cm and \(\Delta t = 10^{-3}\) \(\mu s\). Dirichlet boundary conditions are used where velocity is specified to be zero. Discontinuous initial conditions are given for density and total energy. For the left half of the domain \(\rho = 2.2\) \(g/cm^3\) and \(E = 0.004\) Mbar resulting in a pressure of \(p = 5\) GPa and temperature of \(T = 590\) K. The right half of the domain is set to ambient conditions where \(\rho = \rho_0 = 1.89\) \(g/cm^3\) and \(E = 0.00\) Mbar resulting in a pressure of \(p = 0\) GPa and temperature of \(T = 295\) K. Velocity is initially zero and the sample is purely solid with a mass fraction of unity. Numerical results are shown in Figs. 3 and 4 at time steps of \(t = 0.2\) \(\mu s\) for a duration of one microsecond. Figure 3 shows the density of the sample. As the solution progresses a rarefaction wave, contact discontinuity, and shock wave form. The shock wave travels through the right side of the domain with a value of \(\rho = 2.07\) \(g/cm^3\). Behind the shock and discontinuity, the initial density drops to a value of \(\rho = 2.04\) \(g/cm^3\) as the solution evolves. At time \(t = 1\) \(\mu s\), the rarefaction wave is located at 0.1 cm, the contact discontinuity is located at 0.53 cm and the shock wave is located at 0.85 cm. Velocity reaches a maximum of \(u = 0.03\) cm/\(\mu s\) during the simulation. Figure 4 shows the pressure of the HMX sample. The initial pressure drops from \(p = 5\) GPa to \(p = 2.13\) GPa and is maintained through the shock front. The initial shock conditions are not drastic enough to initiate detonation of the sample within
the simulated duration of $t = 1 \mu s$. The mass fraction never falls below $N_A = 0.99$ and the material remains inert. The computed shock velocity of the system is $0.36 \text{ cm/} \mu \text{s}$ ($p = 5 \text{ GPa}$) and agrees with values reported in literature for experiments with HMX particle composites. Shot # 1120 in Ref. [28] reports a shock velocity of $0.39 \text{ cm/} \mu \text{s}$ for an input pressure of $p = 4.91 \text{ GPa}$.

Next, detonation of 1 cm by 1 cm HMX sample is studied. A uniform mesh with a $\Delta x = \Delta y = 0.01 \text{ cm}$ and $\Delta t = 10^{-4} \mu \text{s}$ is used for a duration of $t = 0.45 \mu \text{s}$. No-slip boundary conditions are considered; i.e. $u = 0$ at $x = [0, 1] \text{ cm}$ and $v = 0$ at $y = [0, 1] \text{ cm}$. A circular detonation front was used with the initial discontinuity located at $r = 0.1 \text{ cm}$. The combustion front is represented as a quarter of a circle that expands as the detonation proceeds. Within the quarter circle the material is shocked to a pressure of $p = 55 \text{ GPa}$ and temperature of $T = 2100 \text{ K}$. Outside, the domain is set to ambient conditions. Figure 5 shows the temperature profile at $t = 0.4 \mu \text{s}$. The temperature wave reaches a maximum value of $T = 3300 \text{ K}$ and is sufficient enough to prompt detonation. Along the $45^\circ$ plane shown in Fig. 5 the burn fraction of the material $\lambda$ is plotted at time intervals of $t = 0.045 \mu \text{s}$ in Fig. 6. Within $t = 0.045 \mu \text{s}$ the solid within the quarter circle is fully burnt. As the solution progresses the shock wave travels through the solid HMX sample and becomes fully gaseous. The calculated shock speed of 1.53 cm/μs is much higher than the previous inert case due to detonation.

This paper presented the one-step second-order Taylor–Galerkin finite element scheme for modeling detonation of HMX via benchmark cases. The integrated algorithm incorporates a high resolution shock capturing scheme, multiple equations of state, Arrhenius kinetics, and mixing rules for HMX detonation simulations. In the detonation model, a one-step reaction scheme was used and temperature and pressure equilibrium between partially reacted states was enforced with a Newton–Raphson method and rule of mixtures. The numerical scheme was tested and agreed with exact solutions for SOD shock tube problem. The test was repeated for a single HMX sample and we showed that the shock velocity compared well with the experimental range reported in literature. Future work will include adding equations for a polymeric binder to simulate detonation in particulate composite microstructures.

Acknowledgments

This paper was based upon work supported by the National Science Foundation Graduate Research Fellowship Program (DGE 1256260) and The Defense Threat Reduction Agency (HDTRA1-31-1-0009).

Appendix A. Supplementary data

Supplementary material related to this article can be found online at http://dx.doi.org/10.1016/j.taml.2016.05.002.

References


