

THE VECTOR FIELD HISTOGRAM - FAST OBSTACLE AVOIDANCE FOR MOBILE ROBOTS

by

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ABSTRACT

A new real-time obstacle avoidance method for mobile robots has been developed and implemented. This method, named the *vector field histogram* (VFH), permits the detection of unknown obstacles and avoids collisions while simultaneously steering the mobile robot toward the target.

The VFH method uses a two-dimensional Cartesian *histogram grid* as a world model. This world model is updated continuously with range data sampled by on-board range sensors. The VFH method subsequently employs a *two-stage* data-reduction process in order to compute the desired control commands for the vehicle. In the first stage the *histogram grid* is reduced to a one-dimensional *polar histogram* that is constructed around the robot's momentary location. Each sector in the *polar histogram* contains a value representing the *polar obstacle density* in that direction. In the second stage, the algorithm selects the most suitable sector from among all *polar histogram* sectors with a low *polar obstacle density*, and the steering of the robot is aligned with that direction.

Experimental results from a mobile robot traversing densely cluttered obstacle courses in smooth and continuous motion and at an average speed of 0.6–0.7m/sec demonstrate the power of the VFH method.

1. INTRODUCTION

Obstacle avoidance is one of the key issues to successful applications of mobile robot systems. All mobile robots feature some kind of collision avoidance, ranging from primitive algorithms that detect an obstacle and stop the robot short of it in order to avoid a collision, through sophisticated algorithms, that enable the robot to detour obstacles. The latter algorithms are much more complex, since they involve not only the detection of an obstacle, but also some kind of quantitative measurements concerning the dimensions of the obstacle. Once these have been determined, the obstacle avoidance algorithm needs to steer the robot around the obstacle and proceed toward the original target. Usually, this procedure requires the robot to stop in front of the obstacle, take the measurements, and only then resume motion. Obstacle avoidance (also called reflexive obstacle avoidance or local path planning) may result in non-optimal paths [5], since no prior knowledge about the environment is used.

A brief survey of relevant earlier obstacle avoidance methods is presented in Section 2, while Section 3 summarizes the *virtual force field*(VFF), an obstacle avoidance method developed earlier by our group at the University of Michigan [5]). While the VFF method provides superior real-time obstacle avoidance for fast mobile robots, some limitations concerning fast travel among densely cluttered obstacles were identified in the course of our experimental work [18]. To overcome these limitations, we developed a new method, named *vector field histogram*(VFH), which is introduced in Section 4. The VFH method eliminates the shortcomings of the VFF method, yet retains all advantages of its predecessor (as will be shown in Section 4). A comparison of the VFH method to earlier methods is given in Section 5, and Section 6 presents experimental results obtained with our VFH-controlled mobile robot.

2. SURVEY OF EARLIER OBSTACLE AVOIDANCE METHODS

This section summarizes relevant obstacle avoidance methods, namely *edge-detection*, *certainty grids*, and *potential field methods*

2.1 Edge-Detection Methods

One popular obstacle avoidance method is based on *edge-detection*. In this method, an algorithm tries to determine the position of the vertical edges of the obstacle and then steer the robot around either one of the "visible" edges. The line connecting two visible edges is considered to represent one of the boundaries of the obstacle. This method was used in our very early research [4], as well as in several other works [11,21,22,28], all using ultrasonic sensors for obstacle detection. A disadvantage with current implementations of this method is that the robot stops in front of obstacles to gather sensor information. However, this is not an

inherent limitation of *edge-detection* methods; it may be possible to overcome this problem with faster computers in future implementations.

In another *edge-detection* approach (using ultrasonic sensors), the robot remains stationary while taking a panoramic scan of its environment [13,14]. After the application of certain line-fitting algorithms, an edge-based *global path planner* is instituted to plan the robot's subsequent path.

A common drawback of both *edge-detection* approaches is their sensitivity to sensor accuracy. Ultrasonic sensors present many shortcomings in this respect:

Poor directionality limits the accuracy in determining the spatial position of an edge to 10-50 cm, depending on the distance to the obstacle and the angle between the obstacle surface and the acoustic axis.

Frequent misreadings are caused by either ultrasonic noise from external sources or stray reflections from neighboring sensors (i.e., crosstalk). Misreadings cannot always be filtered out and they cause the algorithm to falsely detect edges.

Specular reflections occur when the angle between the wavefront and the normal to a smooth surface is too large. In this case the surface reflects the incoming ultra-sound waves away from the sensor, and the obstacle is either not detected, or "seen" as much smaller than it is in reality (since only part of the surface is detected).

Any one of these errors can cause the algorithm to determine the existence of an edge at a completely wrong location, oftentimes resulting in highly unlikely paths.

2.2 The Certainty Grid for Obstacle Representation

A method for probabilistic representation of obstacles in a grid-type world model has been developed at Carnegie-Mellon University (CMU) [13,23,24]. This world model, called *certainty grid*, is especially suited to the accommodation of inaccurate sensor data such as range measurements from ultrasonic sensors.

In the *certainty grid*, the robot's work area is represented by a two-dimensional array of square elements, denoted as cells. Each cell contains a *certainty value* (CV) that indicates the measure of confidence that an obstacle exists within the cell area. With the CMU method, CVs are updated by a probability function that takes into account the characteristics of a given sensor. Ultrasonic sensors, for example, have a conical field of view. A typical ultrasonic sensor [25] returns a radial measure of the distance to the nearest object within the cone, yet does not specify the *angular* location of the object. (Fig. 1 shows the area A in which an object must be located in order to result in a distance measurement d). If an object is detected

by an ultrasonic sensor, it is *more likely* that this object is *closer* to the acoustic axis of the sensor than to the periphery of the conical field of view [4]. For this reason, CMU's probabilistic function C_x increases CVs in cells close to the acoustic axis more than CVs in cells at the periphery.

In CMU's applications of this method [23,24], the mobile robot remains *stationary* while it takes a panoramic scan with its 24 ultrasonic sensors. Next, the probabilistic function C_x is applied to each of the 24 range readings, updating the *certainty grid*. Finally, the robot moves to a new location, stops, and repeats the procedure. After the robot traverses a room in this manner, the resulting *certainty grid* represents a fairly accurate map of the room. A global path-planning method is then employed for off-line calculations of subsequent robot paths.

2.3 Potential Field Methods

The idea of imaginary forces acting on a robot has been suggested by Khatib [16]. In this method, obstacles exert repulsive forces, while the target applies an attractive force to the robot. A resultant force vector \mathbf{R} , comprising the sum of a target-directed attractive force and repulsive forces from obstacles, is calculated for a given robot position. With \mathbf{R} as the *accelerating force* acting on the robot, the robot's new position for a given time interval is calculated, and the algorithm is repeated.

Krogh [19] has enhanced this concept further by taking into consideration the robot's velocity in the vicinity of obstacles. Thorpe [27] has applied the potential field method to off-line path planning and Krogh and Thorpe [20] suggest a combined method for global and local path planning, which uses a "Generalized Potential Field" approach. Newman and Hogan [15] introduce the construction of potential functions through combining individual obstacle functions with logical operations.

Common to these methods is the assumption of a *known and prescribed* world model, in which simple, predefined geometric shapes represent obstacles and the robot's path is generated *off-line*.

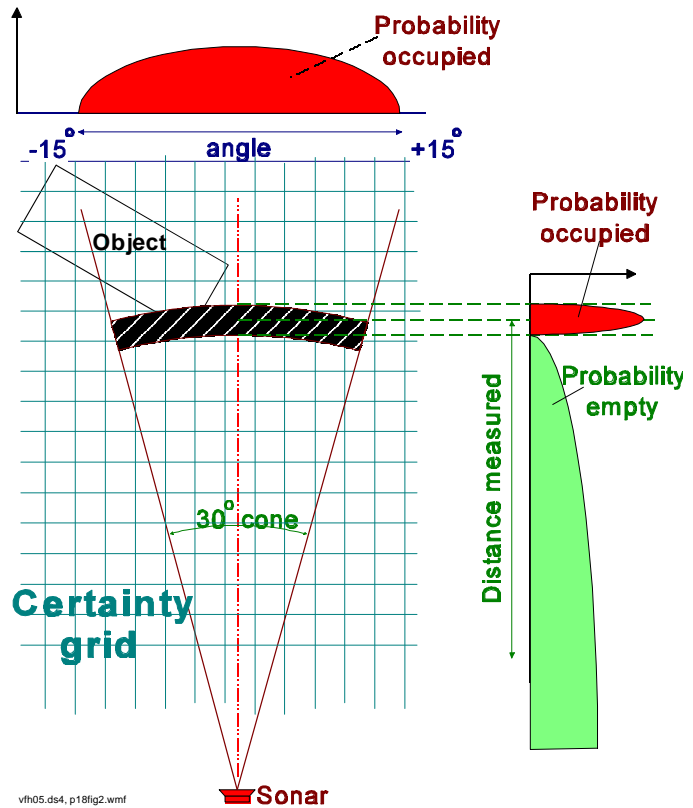


Figure. 1: Two-dimensional projection of the conical field of view of an ultrasonic sensor. A range reading d indicates the existence of an object somewhere within the shaded region A (Carnegie Mellon's method).

While each of the above methods features valuable refinements, none have been implemented on a mobile robot with real sensory data. By contrast, Brooks [8,9] and Arkin [1] use a potential field method on experimental mobile robots (equipped with a ring of ultrasonic sensors). Brooks' implementation treats each ultrasonic range reading as a repulsive force vector. If the magnitude of the sum of the repulsive forces exceeds a certain threshold, the robot stops, turns into the direction of the resultant force vector, and moves on. In this implementation, however, only one set of range readings is considered, while previous readings are lost. Arkin's robot employs a similar method; his robot was able to traverse an obstacle course at 0.12 cm/sec (0.4 feet/sec).

3. THE VIRTUAL FORCE FIELD (VFF) METHOD

The *Virtual Force Field*(VFF) method is our *earlier* real-time obstacle avoidance method for fast-running vehicles [5]. Unlike the methods reviewed above, the VFF method allows for fast, continuous, and smooth motion of the controlled vehicle among unexpected obstacles, and does not require the vehicle to stop in front of obstacles.

3.1 The VFF Concept

The individual components of the VFF method are presented below.

- a. The VFF method uses a two-dimensional Cartesian *histogram grid* \mathbf{C} for obstacle representation. Like in CMU's *certainty grid* concept, each cell (i,j) in the *histogram grid* holds a certainty value, $c_{i,j}$, that represents the confidence of the algorithm in the existence of an obstacle at that location.

The *histogram grid* differs from the *certainty grid* in the way it is built and updated. CMU's method projects a probability profile onto those cells that are affected by a range reading; this procedure is computationally intensive and would impose a heavy time-penalty if real-time execution on an on-board computer was attempted. Our method, on the other hand, increments only one cell in the *histogram grid* for each range reading, creating a "*probability*" *distribution*¹ with only small computational overhead. For ultrasonic sensors, this cell corresponds to the measured distance d (see Fig. 2a) and lies on the acoustic axis of the sensor. While this approach may seem to be an oversimplification, a *probabilistic* distribution is actually obtained by *continuously* and *rapidly* sampling each sensor while the vehicle is moving. Thus, the same cell and its neighboring cells are repeatedly incremented, as shown in Fig. 2b. This results in a *histogramic probability distribution*, in which high *certainty values* are obtained in cells close to the actual location of the obstacle.

¹ We use the term "probability" in the literal sense of "*likelihood*."

b. Next, we apply the potential field idea to the *histogram grid*, so the *probabilistic* sensor information can be used efficiently to control the vehicle. Fig. 3 shows how this algorithm works:

As the vehicle moves, a window of $w_s \times w_s$ cells accompanies it, overlying a square region of C . We call this region the "*active region*" (denoted as C^*), and cells that momentarily belong to the *active region* are called "*active cells*" (denoted as $c_{i,j}^*$). In our

current implementation, the size of the window is 33×33 cells (with a cell size of $10\text{cm} \times 10\text{cm}$), and the window is always centered about the robot's position. Note that a *circular* window would be geometrically more appropriate, but is computationally more expensive to handle than a *square* one.

Each *active cell* exerts a *virtual repulsive force* $F_{i,j}$ toward the robot. The magnitude of this force is proportional to the certainty value $c_{i,j}^*$ and inversely proportional to d^x , where d is the distance between the cell and the center of the vehicle, and x is a positive real number (we assume $x=2$ in the following discussion). At each iteration, all virtual repulsive forces are added up to yield the resultant repulsive force F_r . Simultaneously, a virtual attractive force F_t of constant magnitude is applied to the vehicle, "pulling" it toward the target. The summation of F_r and F_t yields the resulting force vector R . In order to compute R , up to $33 \times 33 = 1089$ individual repulsive force vectors $F_{i,j}$ must be computed and accumulated. The computational heart of the VFF algorithm is therefore a specially developed algorithm for the fast computation and summation of the repulsive force vectors.

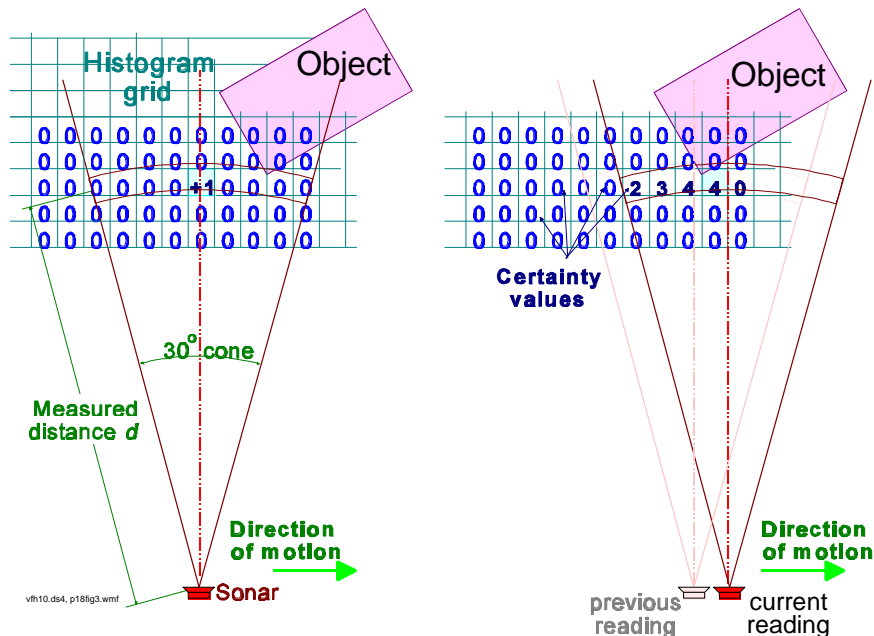


Figure 2:
a. Only one cell is incremented for each range reading. With ultrasonic sensors, this is the cell that lies on the acoustic axis and corresponds to the measured distance d .
b. A *histogram probability distribution* is obtained by continuous and rapid sampling of the sensors while the vehicle is moving

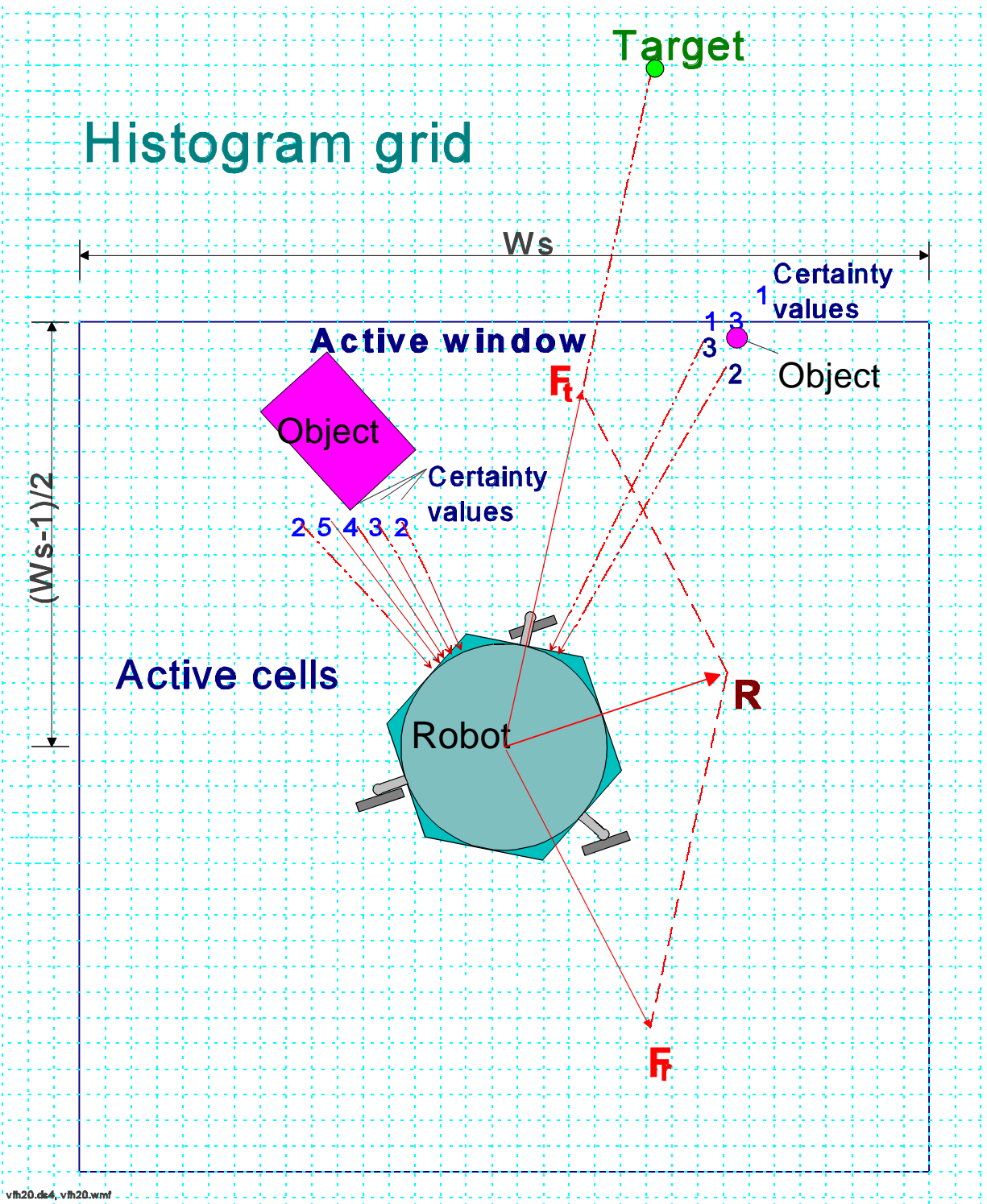


Figure 3: The Virtual Force Field (VFF) concept: Occupied cells exert repulsive forces onto the robot; the magnitude is proportional to the certainty value $c_{i,j}$ of the cell and inversely proportional to d^2 .

- c. Combining the above two concepts (a.) and (b.) in real-time enables sensor data to influence the steering control *immediately*. In practice, each range reading is recorded into the *histogram grid* as soon as it becomes available, and the subsequent calculation of \mathbf{R} takes this data-point into account. This feature gives the vehicle fast response to obstacles that appear suddenly, resulting in fast reflexive behavior imperative at high speeds.

3.2 Shortcomings of the VFF Method

The VFF method has been implemented and extensively tested on-board a mobile robot equipped with a ring of 24 ultrasonic sensors (see Section 6). Under most conditions, the VFF-controlled robot performed very well. Typically, it traversed an obstacle course at an average speed of 0.5m/sec, provided the obstacles were placed at least 1.8m apart (the robot diameter is 0.8m). With less clearance between two obstacles (e.g., a doorway), some problems were encountered. Sometimes, the robot would not pass through a doorway, because the repulsive forces from both sides of the doorway resulted in a force that pushed the robot away.

Another problem arose out of the discrete nature of the *histogram grid*. In order to efficiently calculate repulsive forces in real-time, the robot's momentary position is mapped onto the *histogram grid*. Whenever this position changes from one cell to another, drastic changes in the resultant \mathbf{R} may be encountered. The following numeric example explains this point. Consider a repulsive force generated by a cell (m,n) and applied to the robot's momentary position at $(m,n+6)$, which is six cells away (i.e., 0.6 m, with a cell size of 10x10cm). The magnitude of this particular force vector is $|\mathbf{F}_{m,n}|=k/0.6^2=2.8k$. As the robot advances by one cell, and its position corresponds to cell $(m,n+5)$, the new force vector is $|\mathbf{F}'_{m,n}|=k/0.5^2=4k$. The change is 42%. Changes of this magnitude cause considerable fluctuations in the steering control. The situation is even worse when the magnitude of the target-directed constant attractive force \mathbf{F}_t lies between the directions of the two successive forces $|\mathbf{F}|$ and $|\mathbf{F}'|$ (this condition is in fact most likely, because it corresponds to the "steady state" condition when the robot travels alongside an obstacle). In this situation, the direction of the resultant \mathbf{R} may fluctuate by up to 180°. For this reason it is necessary to smooth the control signal to the steering motor by adding a low-pass filter to the VFF control loop [5]. This filter, however, introduces a delay that adversely affects the robot's steering response to unexpected obstacles.

Finally, we also identified a problem that occurs when the robot travels in narrow corridors. When traveling along the center-line between the two corridor walls, the robot's motion is stable. If, however, the robot strays slightly to either side of the center-line, it experiences a strong virtual repulsive force from the closer wall. This force usually "pushes" the robot across the center-line, and the process repeats with the other wall. Under certain conditions, this process results in oscillatory and unstable motion [17,18].

4. THE VECTOR FIELD HISTOGRAM (VFH) METHOD

Careful analysis of the shortcomings of the VFF method reveals its inherent problem: excessively drastic data reduction that occurs when the individual repulsive forces from *histogram grid* cells are added up to calculate the resultant force vector F_r . Hundreds of data points are reduced in one step to only two items: direction and magnitude of F_r . Consequently, *detailed information about the local obstacle distribution is lost*

To remedy this shortcoming, we have developed a new method called the *vector field histogram* (VFH). The VFH method employs a *two-stage data reduction* technique, rather than the single-step technique used by the VFF method. Thus, three levels of data representation exist:

- a. The highest level holds the detailed description of the robot's environment. In this level, the two-dimensional Cartesian *histogram grid* C is continuously updated in real-time with range data sampled by the on-board range sensors. This process is identical to the one described in Section 3 for the VFF method.
- b. At the intermediate level, a one-dimensional *polar histogram* H is constructed around the robot's momentary location. H comprises n angular sectors of width α . A transformation (described in Section 4.1, below) maps the *active region* C^* onto H , resulting in each sector k holding a value h_k that represents the *polar obstacle density* in the direction that corresponds to sector k .
- c. The lowest level of data representation is the output of the VFH algorithm: the reference values for the drive and steer controllers of the vehicle.

The following sections describe the two data reduction stages in more detail.

4.1 First Data Reduction and Creation of the *Polar Histogram*

The first data-reduction stage maps the *active region* C^* of the *histogram grid* C onto the *polar histogram* H , as follows: As with our earlier VFF method, a *window* moves with the vehicle, overlying a square region of $w_s \times w_s$ cells in the *histogram grid* (see Fig. 4). The contents of each *active cell* in the *histogram grid* are now treated as an *obstacle vector*, the direction of which is determined by the direction β from the cell to the *Vehicle Center Point* (VCP)²

² For symmetrically shaped vehicles, the VCP is easily defined as the geometric center of the vehicle. For rectangular vehicles, it is possible to choose two VCPs, e.g., one each at the center-point of the front and rear axles.

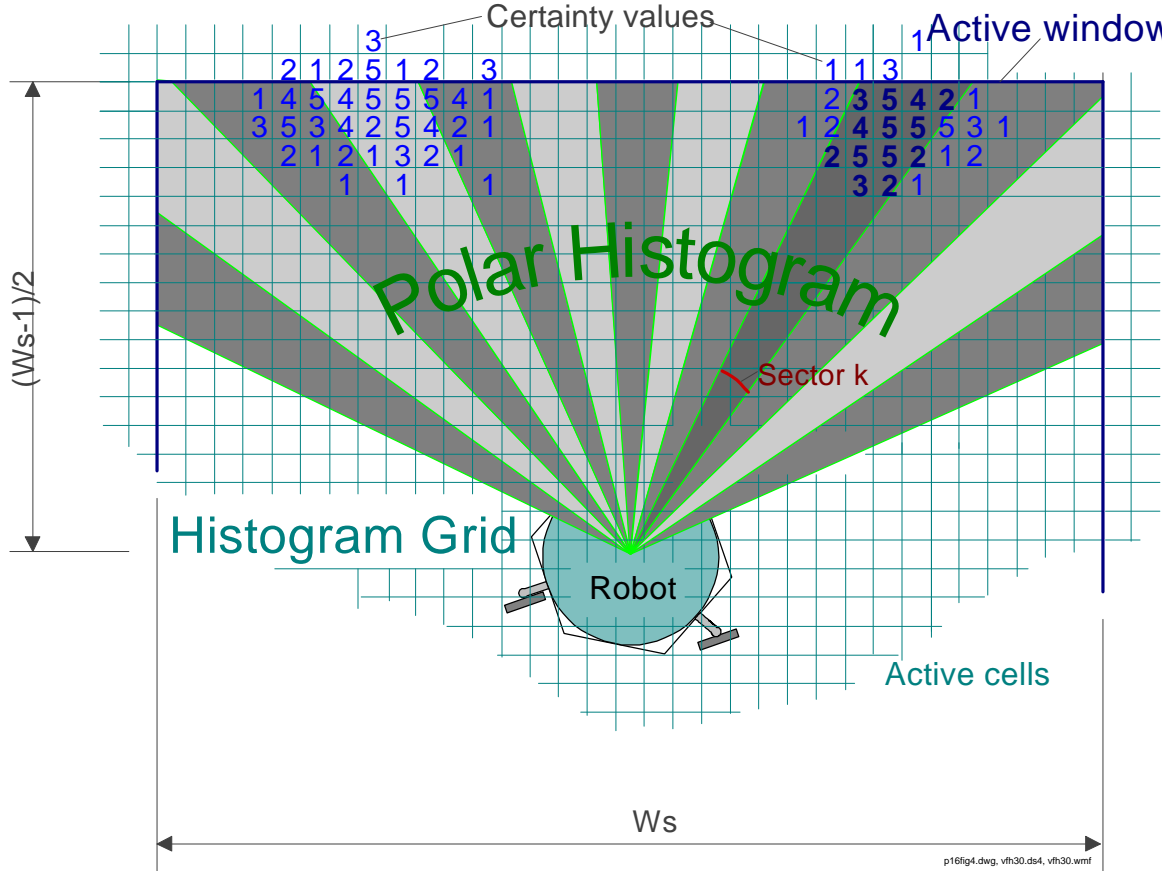


Figure 4: Mapping of active cells onto the polar histogram

$$b_{i,j} = \tan^{-1} \frac{y_i - y_0}{x_i - x_0} \quad (1)$$

and the magnitude is given by

$$m_{i,j} = (c_{i,j}^*)^2 (a - b d_{i,j}) \quad (2)$$

where

- a, b Positive constants.
- $c_{i,j}^*$ Certainty value of active cell (i,j) .
- $d_{i,j}$ Distance between active cell (i,j) and the VCP.
- $m_{i,j}$ Magnitude of the obstacle vector at cell (i,j) .
- x_0, y_0 Present coordinates of the VCP.
- x_i, y_j Coordinates of active cell (i,j) .
- $\beta_{i,j}$ Direction from active cell (i,j) to the VCP.

Notice that

- a. $c_{i,j}^*$ is squared. This expresses our confidence that *recurring* range readings represent actual obstacles, as opposed to single occurrences of range readings, which may be caused by noise.
- b. $m_{i,j}$ is proportional to $-d$. Therefore, occupied cells produce large vector magnitudes when they are in the immediate vicinity of the robot, and smaller ones when they are further away. Specifically, a and b are chosen such that $a-bd_{max}=0$, where $d_{max} = \sqrt{2} (w_s-1)/2$ is the distance between the farthest *active cell* and the VCP. This way $m_{i,j}=0$ for the farthest *active cell* and increases linearly for closer cells.

\mathbf{H} has an arbitrary angular resolution α such that $n=360/\alpha$ is an integer (e.g., $\alpha=5^\circ$ and $n=72$). Each sector k corresponds to a discrete angle ρ quantized to multiples of α , such that $\rho=k\alpha$, where $k = 0,1,2,\dots,n-1$. Correspondence between $c_{i,j}^*$ and sector k is established through

$$k = \text{INT}(\beta_{i,j}/\alpha) \quad (3)$$

For each sector k , the *polar obstacle density* h_k is calculated by

$$h_k = \sum_{i,j} m_{i,j} \quad (4)$$

Each *active cell* is related to a certain sector by equations (1) and (3). In Fig. 4, which shows the mapping from \mathbf{C}^* into \mathbf{H} , all *active cells* related to sector k have been highlighted. Note that the sector width in Fig. 4 is $\alpha=10^\circ$ (not $\alpha=5^\circ$, as in the actual algorithm) to clarify the drawing.

Because of the discrete nature of the *histogram grid*, the result of this mapping may appear ragged and cause errors in the selection of the steering direction (as explained in Section 4.2). Therefore, a smoothing function is applied to \mathbf{H} , which is defined by

$$h'_k = \frac{h_{k-l} + 2h_{k-l+1} + \dots + lh_k + \dots + 2h_{k+l-1} + h_{k+l}}{2l+1} \quad (5)$$

where h'_k is the *smoothed polar obstacle density* (POD).

In our current implementation, $l=5$ yields satisfactory smoothing results.

Fig. 5a shows a typical obstacle setup in our lab. Note that the gap between obstacles B and C is only 1.2m and that A is a thin pole of 3/4" diameter. The *histogram grid* obtained after partially traversing this obstacle course is shown in Fig. 5b. The (smoothed) *polar histogram* corresponding to the momentary position of the robot O is shown in Fig. 6a. The directions

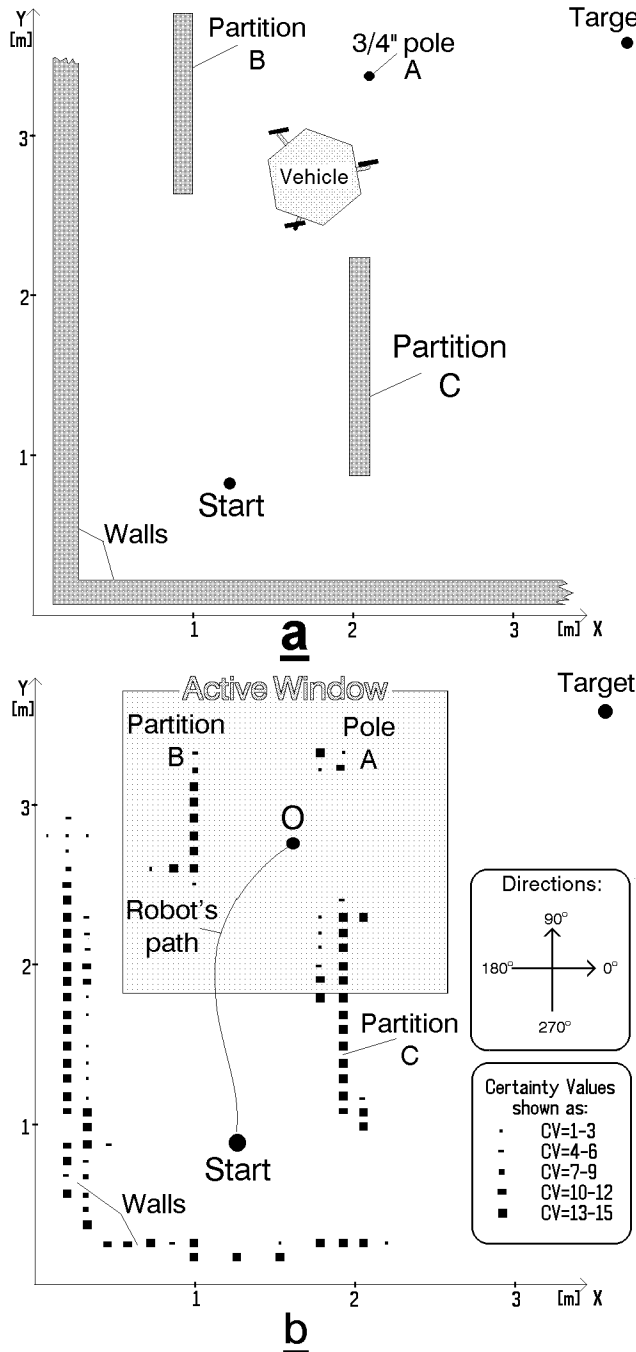


Figure 5: a. Example of an obstacle course.
b. The corresponding *Histogram grid* representation.

(in degrees) in the *polar histogram* correspond to directions measured counterclockwise from the positive x-axis of the *histogram grid*. The peaks A, B, and C in the *polar histogram* result from obstacle clusters A, B, and C in the *histogram grid*. Fig. 6b shows the *polar form* of the exact same *polar histogram* as Fig. 6a, overlaying part of the *histogram grid* of Fig. 5b.

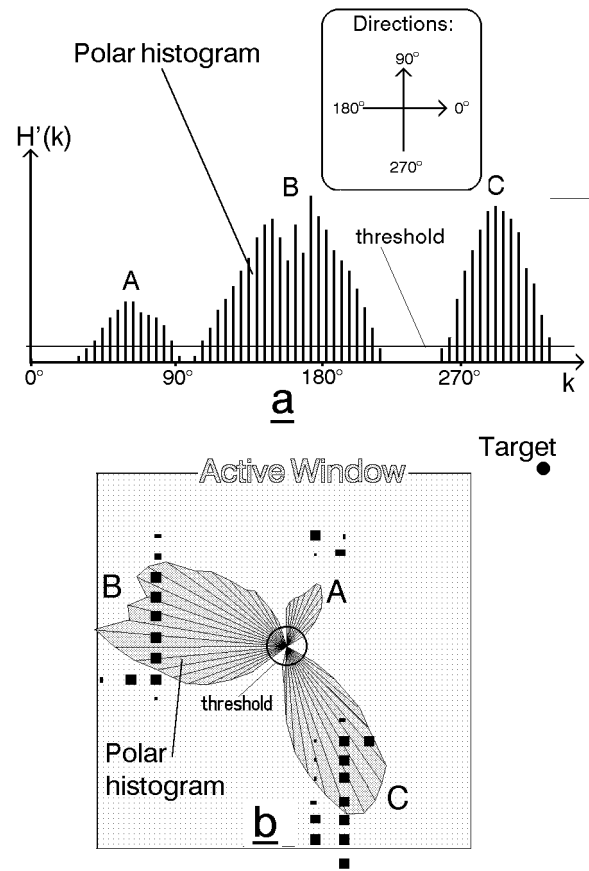
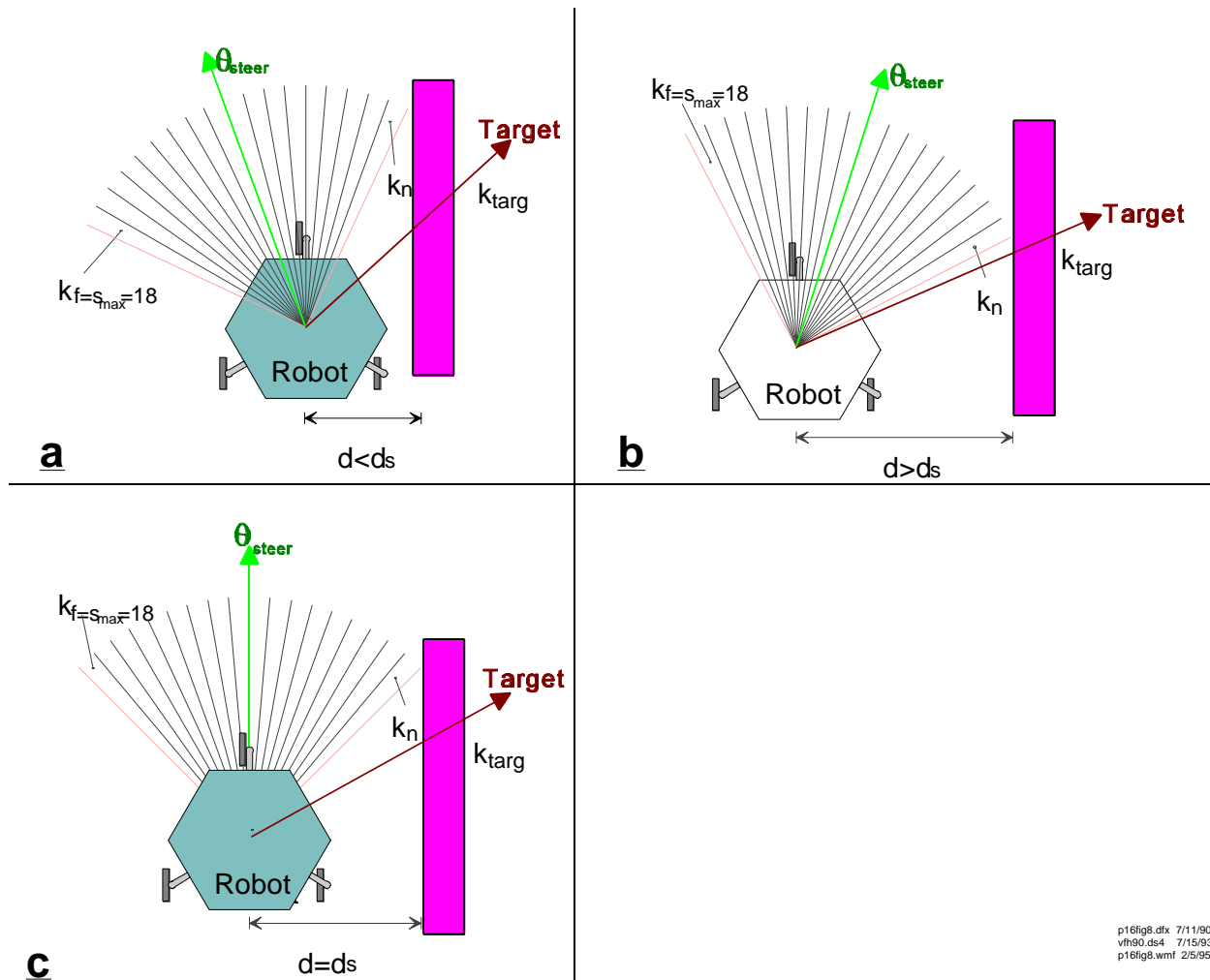


Figure 6:
a. *Polar obstacle density* represented in the *smoothed polar histogram* $H'(k)$ relative to the robot's position at O (in Fig. 5b).
b. The same *polar histogram* as in a, shown in *polar form* and overlaying part of the *histogram grid* of Fig. 5b.



p16fig8.dtx 7/11/90
vfh90.ds4 7/15/93
p16fig8.wmf 2/5/95

Figure 8: Obtaining a stable path when traveling alongside an obstacle:
a. θ points away from the obstacle when the robot is too close.
b. θ points toward the obstacle when the robot is further away.
c. Robot runs alongside the obstacle when at the proper distance d_s .

steady state conditions.

The second case, a *narrow valley*, is created when the mobile robot travels between closely spaced obstacles, as shown in Fig. 9. Here the *far border* k_f is less than s_{max} sectors apart from k_n . However, the direction of travel is again chosen as $\theta = (k_n + k_f)/2$ and the robot maintains a course centered between obstacles.

Note that the robot's ability to pass through narrow passages and doorways results from the ability to identify a *narrow valley* and to choose a centered path through that *valley*. This feature is made possible through the intermediate data representation in the *polar histogram*. Our earlier VFF method and other potential field methods, by contrast, lack this ability [18].

- b. If, on the other hand, the threshold is much too low, some potential *candidate valleys* will be precluded and the robot will not pass through narrow passages.

In summary, it can be concluded that the VFH-system needs a fine-tuned threshold only for the most challenging applications (e.g., travel at high speed *and* in densely cluttered environments); under less demanding conditions the system performs well even with an unprecisely set threshold.

One way to optimize performance is to set an *adaptive threshold* from a higher hierarchical level, e.g., as a function of a "global" plan. For example, during normal travel the threshold is set to a very safe, low level. If the global plan calls for passing through a narrow passage (e.g., a doorway), the threshold is temporarily raised while the travel speed is lowered.

4.4 Speed Control

The robot's maximum speed V_{max} can be set at the beginning of a run. The robot tries to maintain this speed during the run unless forced by the VFH algorithm to a lower instantaneous speed V , which is determined in each sampling interval as follows:

The *smoothed polar obstacle density* in the *current* direction of travel is denoted as h'_c . $h'_c > 0$ indicates that an obstacle lies ahead of the robot. Large values of h'_c mean a large obstacle lies ahead or an obstacle is very close to the robot. Either case is likely to require a drastic change in direction, and a reduction in speed is necessary to allow the steering wheels to turn into the new direction. This reduction in speed is implemented by the following function:

$$V' = V_{max} (1 - h'_c/h_m) \quad (8)$$

where

$$h'_c = \min(h'_c, h_m) \quad (9)$$

and h_m is an empirically determined constant that causes a sufficient reduction in speed. Note that Eq. (9) guarantees $V' \geq 0$, since $h'_c \leq h_m$.

While Eqs. (8) and (9) reduce the speed of the robot in *anticipation* of a steering maneuver, speed can be further reduced proportionally to the actual steering rate Ω :

$$V = V'(1 - \Omega/\Omega_{max}) + V_{min} \quad (10)$$

where Ω_{max} is the maximal allowable steering rate for the mobile robot (in our system $\Omega_{max} = 120^\circ/\text{sec}$).

Note that V is prevented from going to zero by setting a lower limit for V , namely $V \geq V_{min}$; in our implementation $V_{min} = 4\text{cm}/\text{sec}$.

4.5 Limitations and Remedies

The VFH method is a *local path planner*, i.e., it does not attempt to find an *optimal path* (an optimal path can only be found if complete environmental information is given). Furthermore, a VFH controlled robot may get "trapped" in dead-end situations (as is the case with other *local path planners*). When trapped, mobile robots usually exhibit what has been called "*cyclic behavior*," i.e., going around in circles or cycling between *multiple traps* (typical examples for *cyclic behavior* are discussed in [5]). While it is possible to devise a set of heuristic rules that would guide the robot out of *trap-situations* and resolve *cyclic behavior* [5], the resulting path is still not optimal.

To resolve these problems, we have introduced a *path monitor* that works as follows: If the robot diverts from the target direction k_{targ} (see Fig. 9) the *path monitor* records this as either left (as is the case in Fig. 9) or right *diversion mode*. Subsequently, when looking for the *near* border of the closest *candidate valley*, k_n (see Section 4.2), the VFH algorithm searches to the *left* or *right* of k_{targ} , according to the original *diversion mode*. If k_n cannot be found within $n=180^\circ/\alpha=36$ sectors, the *path monitor* flags a *trap-situation*. Once a certain *diversion mode* has been set, it is only cleared if the robot faces again into the target direction.

When a *trap-situation* is flagged, the robot slows down (and may come to a complete halt), while the VFH algorithm is temporarily suspended. A *global path planner* (GPP) algorithm is then invoked to plan a new path based on the available information in the *histogram grid* [29]. The new path comprises a set of *via-points* that are then presented as intermediate target locations to the VFH algorithm.

The maximum travel speed of a VFH-controlled robot is limited by the sampling rate of the ultrasonic sensors, and not by the computation time of the algorithm. In our system, it takes 160 msec to have all 24 ultrasonic sensors sampled and processed once. We estimate that with our current computing hardware (see Section 6) a travel speed of up to 1.5m/sec is possible if the sampling rate of the sensors could be doubled. The relationship between sampling time, robot travel speed, signal-to-noise ratio, and the resulting certainty values is rather complicated and cannot be treated here because of space limitations (a thorough discussion of this problem is given in [6] and [7]).

5. COMPARISON TO EARLIER METHODS

During our research in obstacle avoidance for mobile robots [2,3,4,5] we implemented and evaluated some of the methods discussed in Section 2. This section compares the performance of our new VFH method to these earlier methods.

5.1 Comparison to Edge-Detection Methods

The blurry and inaccurate data produced by ultrasonic sensors does not provide the sharply defined contours required by *edge-detection* methods. Consequently, misreadings or inaccurate range measurements may be interpreted as part of an obstacle, thereby distorting the perceived shape of the obstacle.

The VFH method, on the other hand, reacts to clusters of range readings. As soon as a range reading has been sampled, it becomes available to the steering controller (via the *histogram grid*) and can influence the path of the vehicle immediately. A single range reading will have only minor influence on the path, while repeated range readings in a confined area (cluster) will cause a more drastic change of direction for the vehicle.

The force field method developed by Brooks [8,9] and the similar method developed by Arkin [1], do function in *experimental* real-time systems, using actual sensory data [8,9]. However, these methods are somewhat oversimplified, since a threshold determines if an object is at a safe distance or too close. In the latter case, and because of the binary character of the threshold, the robot must stop and rotate away from the object before resuming motion. An additional shortcoming of these methods is their susceptibility to misreadings (due to ultrasonic noise, crosstalk, etc.) since they take into account only one set of range readings (one reading from each ultrasonic sensor). Consequently, misreadings and correct readings (i.e., those produced by actual obstacles) have the same weight. Therefore, a single misreading can cause the resultant force to exceed the threshold level and "scare" the robot away from a possibly safe, free path. Our method, on the other hand, also takes into account *past* measurements by means of the *histogram grid*, thereby increasing the weight of recurring measurements, while minimizing the weight of randomly occurring misreadings. In addition, the *smoothing function* (Eq. 5) reduces the weight of false readings. Thus, the VFH method results in much more robust and error-resistant control. An additional advantage of the VFH method is the permanent map information contained in the *histogram grid* after a run. Brooks' and Arkin's methods, on the other hand, do not produce a permanent record.

A critical discussion of both *simulated* and *experimental* potential field methods is given in [18]. Also, based on a rigorous mathematical analysis, [18] discusses six inherent shortcomings of potential field methods.

5.4 Reflexive vs. Reactive Control

On a more abstract level, researchers are beginning to distinguish between two fundamentally different approaches to mobile robot obstacle avoidance. The "conventional" approach, *reactive* control, is based on the traditional artificial intelligence model of human *cognition*. *Reactive* control algorithms reason about the robot's *perception* (sensor data) while building elaborate world models (memory) and subsequently plan the robot's *actions*. This approach requires large amounts of computation and decision making, resulting in a relatively slow

CARMEL is equipped with a ring of 24 ultrasonic sensors [25]. The sensor ring has a diameter of 0.8m, and objects must be at least 0.27m away from the sensors to be detected. Therefore, the theoretical minimum width for safe travel in a passage-way is

$$W_{min}=0.8 + 2 \times 0.27 = 1.34 \text{ m.}$$

In extensive tests, we ran the VFH-controlled CARMEL through difficult obstacle courses. The obstacles were unmarked, commonplace objects such as chairs, partitions, and bookshelves. In most experiments, CARMEL ran at its maximum speed $V_{max}=0.78\text{m/sec}$. This speed was only reduced when an obstacle was approached head-on (see discussion of speed control in Section 4.4).

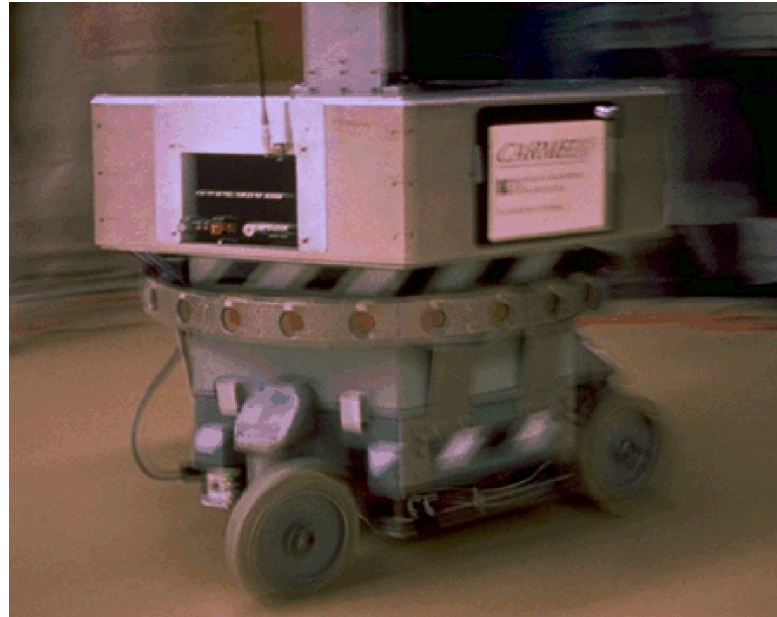


Figure 10: CARMEL, The University of Michigan's Cybermotion K2A robot, dashes through an obstacle course at 0.8 m/sec.

Fig. 11 shows the *histogram grid* after a run through a particularly challenging obstacle course of 3/4"-diameter vertical poles spaced at a distance of about 1.4m from each other. The actual location of the rods is indicated by (+) symbols in Fig. 11. It should be noted that none of the obstacle locations were known to the robot in advance: the CV-clusters in Fig. 11 gradually appeared on the operator's screen while CARMEL was moving.

To test the performance limits of our system, we performed a variety of experiments with other slender obstacles. For example, 1/2" diameter poles were still detected, but not reliably so when approached at CARMEL's maximum speed. Unreliable detection would also result when 1"x1" square rods were used. Larger objects, such as 2" diameter cylinders, square shaped cardboard boxes, furniture, and even slowly walking people are reliably detected and avoided. These obstacles are easier to detect than the 3/4" poles in the experiment described here.

Each blob in Fig. 11 represents one cell in the *histogram grid*. In our current implementation, *certainty values*(CVs) range from 0 to 15 and are indicated in Fig. 11 by blobs of varying sizes. CV = 0 means no sensor reading has been projected onto the cell during the run (i.e., no blob), while CVs > 0 indicate the increasing confidence in the existence of an object at that location. CARMEL traversed this obstacle course at an average speed of 0.58 m/sec without stopping for obstacles. Note that this is a *typical* experimental run, and similar performance

has been routinely obtained in countless experiments and demonstrations, using different kinds of obstacles at random layouts.

An indication of the real-time performance of the VFH algorithm is the sampling time T (i.e., the rate at which the steer and speed commands for the low-level controller are issued). The following steps occur during T :

- a. Obtain sonar information from the sensor controller.
- b. Update the *histogram grid*.
- c. Create the *polar histogram*.
- d. Determine the free sector and steering direction.
- e. Calculate the speed command.
- f. Communicate with the low-level motion controller (send speed and steer commands and receive position update).

On an Intel 80386-based PC-compatible computer running at 20 Mhz, $T = 27$ msec.

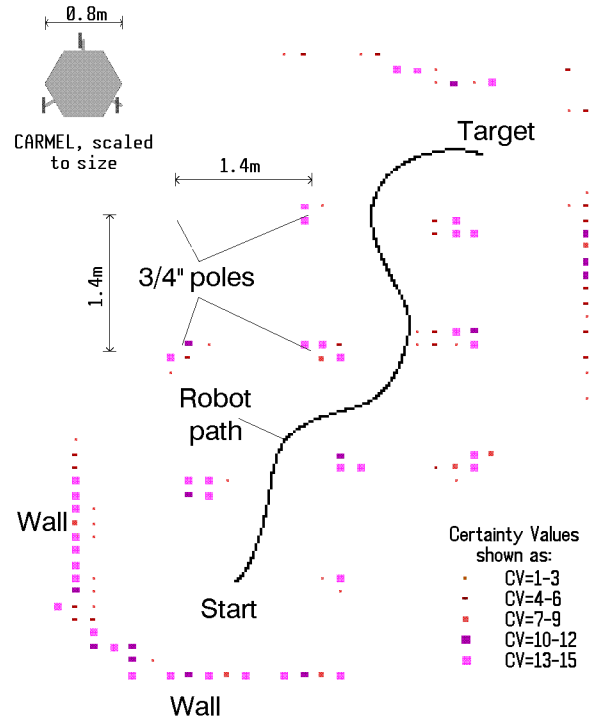
7. CONCLUSIONS

This paper presents a new obstacle avoidance method for fast-running vehicles.

This approach, called the *vector field histogram* (VFH) method, has been developed and successfully tested on our experimental mobile robot CARMEL. The VFH algorithm is computationally efficient, very robust and insensitive to misreadings, and it allows continuous and fast motion of the mobile robot without stopping for obstacles. The VFH-controlled mobile robot traverses very densely cluttered obstacle courses at high average speeds and is able to pass through narrow openings (e.g., doorways) or negotiate narrow corridors without oscillations.

The VFH method is based on the following principles:

- a. A two-dimensional Cartesian *histogram grid* is continuously updated in real-time with range data sampled by the on-board range sensors.
- b. The *histogram grid* is reduced to a one-dimensional *polar histogram* that is constructed around the momentary location of the robot. The *polar histogram* is the most significant



Experimental run through densely cluttered obstacle course.

Average speed = 0.58 m/sec.

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5/7/90

Figure 11: *Histogram grid* representation of a run through a field of densely spaced, thin vertical poles. The average speed in this run was $V_{avg} = 0.58$ m/sec.

8. REFERENCES

1. Arkin, R. C., "Motor Schema-Based Mobile Robot Navigation." *The International Journal of Robotics Research* August 1989, pp. 92-112.
2. Borenstein, J. and Koren, Y., "A Mobile Platform For Nursing Robots." *IEEE Transactions on Industrial Electronics* Vol. 32, No. 2, 1985, pp. 158-165.
3. Borenstein, J. and Koren, Y., "Motion Control Analysis of a Mobile Robot." *Transactions of ASME, Journal of Dynamics, Measurement and Control* Vol. 109, No. 2, 1987, pp. 73-79.
4. Borenstein, J. and Koren, Y., "Obstacle Avoidance With Ultrasonic Sensors." *IEEE Journal of Robotics and Automation* Vol. RA-4, No. 2, 1988, pp. 213-218.
5. Borenstein, J. and Koren, Y., "Real-time Obstacle Avoidance for Fast Mobile Robots." *IEEE Transactions on Systems, Man, and Cybernetics* Vol. 19, No. 5, Sept/Oct 1989, pp. 1179-1187.
6. Borenstein, J. and Koren, Y., "Histogramic In-motion Mapping for Mobile Robot Obstacle Avoidance." *IEEE Journal of Robotics and Automation* Vol. 7, No. 4, 1991, pp. 535-539.
7. Borenstein, J. and Koren, Y., "Real-time Map-building for Fast Mobile Robot Obstacle Avoidance." *SPIE Symposium on Advances in Intelligent Systems, Mobile Robots*, V Boston, MA, Nov. 4-9, 1990.
8. Brooks, R. A., "A Robust Layered Control System for a Mobile Robot." *IEEE Journal of Robotics and Automation* Vol. RA-2, No. 1, 1986, pp. 14-23.
9. Brooks, R. A. and Connell, J. H., "Asynchronous Distributed Control System for a Mobile Robot." *Proceedings of the SPIE, Mobile Robots* Vol. 727, 1987, pp. 77-84.
10. Crowley, J. L., "Dynamic World Modeling for an Intelligent Mobile Robot." *IEEE Seventh International Conference on Pattern Recognition, Proceeding* Montreal, Canada, July 30-August 2, 1984, pp. 207-210.
11. Crowley, J. L., "World Modeling and Position Estimation for a Mobile Robot Using Ultrasonic Ranging." *Proceedings of the 1989 IEEE International Conference on Robotics and Automation* Scottsdale, Arizona, May 14-19, 1989, pp. 674-680.
12. Cybermation, "K2A Mobile Platform." *Commercial Offer*, 5457 JAE Valley Road, Roanoke, VA 24014, 1987.

13. Elfes, A., "Sonar-based Real-World Mapping and Navigation." *IEEE Journal of Robotics and Automation*, Vol. RA-3, No 3, 1987, pp. 249-265.
14. Flynn, A. M., "Combining Sonar and Infrared Sensors for Mobile Robot Navigation." *The International Journal of Robotics Research* Vol. 7, No. 6, December 1988, pp. 5-14.
15. Newman, W. S. and Hogan, N., "High Speed Robot Control and Obstacle Avoidance Using Dynamic Potential Functions." *Proceedings of the 1987 IEEE International Conference on Robotics and Automation*, Raleigh, North Carolina, March 31-April 3, 1987, pp. 14-24.
16. Khatib, O., "Real-Time Obstacle Avoidance for Manipulators and Mobile Robots." *1985 IEEE International Conference on Robotics and Automation*, St. Louis, Missouri, March 25-28, 1985, pp. 500-505.
17. Koren, Y. and Borenstein, J., "Analysis of Control Methods for Mobile Robot Obstacle Avoidance." *Proceedings of the IEEE International Workshop on Intelligent Motion Control*, Istanbul, Turkey, August 20-22, 1990, pp. 457-462.
18. Koren, Y. and Borenstein, J., 1991, "Potential Field Methods and Their Inherent Limitations for Mobile Robot Navigation." *Proceedings of the IEEE International Conference on Robotics and Automation*, Sacramento, California, April 7-12, 1991, pp. 1398-1404.
19. Krogh, B. H., "A Generalized Potential Field Approach to Obstacle Avoidance Control." *International Robotics Research Conference*, Bethlehem, Pennsylvania, August, 1984.
20. Krogh, B. H. and Thorpe, C. E., "Integrated Path Planning and Dynamic Steering Control for Autonomous Vehicles." *Proceedings of the 1986 IEEE International Conference on Robotics and Automation*, San Francisco, California, April 7-10, 1986, pp. 1664-1669.
21. Kuc, R. and Barshan, B., "Navigating Vehicles Through an Unstructured Environment With Sonar." *Proceedings of the 1989 IEEE International Conference on Robotics and Automation*, Scottsdale, Arizona, May 14-19, 1989, pp. 1422-1426.
22. Lumelsky V. and Skewis, T., "A Paradigm for Incorporating Vision in the Robot Navigation Function." *Proceedings of the 1988 IEEE Conference on Robotics and Automation*, Philadelphia, April 25, 1988, pp. 734-739.
23. Moravec, H. P. and Elfes, A., "High Resolution Maps from Wide Angle Sonar." *IEEE Conference on Robotics and Automation*, Washington D.C., 1985, pp. 116-121.

24. Moravec, H. P., "Sensor Fusion in Certainty Grids for Mobile Robots." *AI Magazine*, Summer 1988, pp. 61-74.
25. POLAROID Corporation, Ultrasonic Components Group, 119 Windsor Street, Cambridge, Massachusetts 02139, 1990.
26. Raschke, U. and Borenstein, J., "A Comparisson of Grid-type Map-building Techniques by Index of Performance." *Proceedings of the 1990 IEEE International Conference on Robotics and Automation*, Cincinnati, Ohio, May 13-18, 1990.
27. Thorpe, C. F., "Path Relaxation: Path Planning for a Mobile Robot." *Carnegie-Mellon University, The Robotics Institute, Mobile Robots Laboratory, Autonomous Mobile Robots, Annual Report 1985* pp. 39-42.
28. Weisbin, C. R., de Saussure, G., and Kammer, D., "SELF-CONTROLLED. A Real-Time Expert System for an Autonomous Mobile Robot." *Computers in Mechanical Engineering*, September, 1986, pp. 12-19.
29. Zhao, Y., BeMent, S. L., and Borenstein, J., "Dynamic Path Planning for Mobile Robot Real-time Navigation." *Twelfth IASTED International Symposium on Robotics and Manufacturing*, Santa Barbara, California, November 13-15, 1989.

Footnotes

1. We use the term "*probability*" in the literal sense of "*likelihood*."
2. For symmetrically shaped vehicles, the VCP is easily defined as the geometric center of the vehicle. For rectangular vehicles, it is possible to chose two VCPs, e.g., one each at the center-point of the front and rear axles.